

**R. Ludwig and G. Bogdanov**  
**“RF Circuit Design: Theory and Applications”**  
**2<sup>nd</sup> edition**

**Figures for Chapter 4**

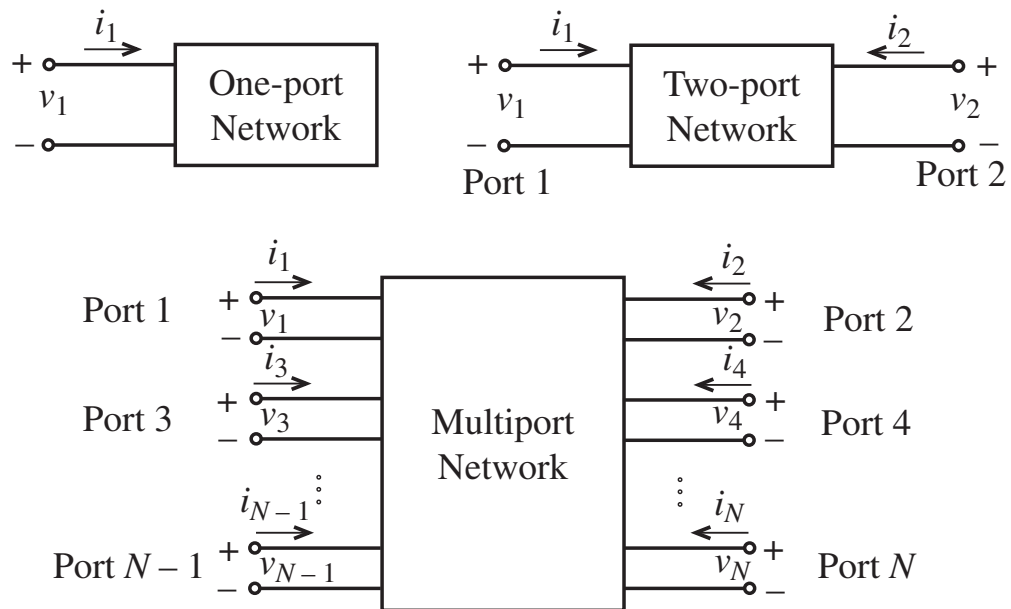


Figure 4-1 Basic voltage and current definitions for single- and multiport network.

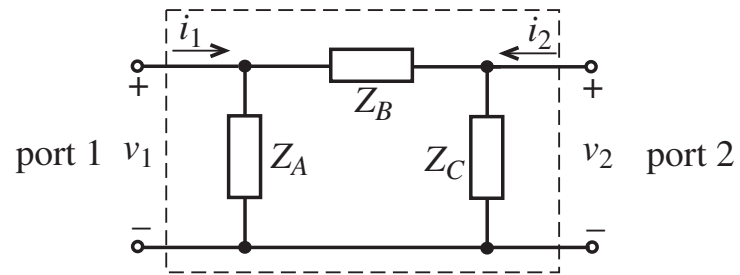


Figure 4-2 Pi-network as a two-port network.

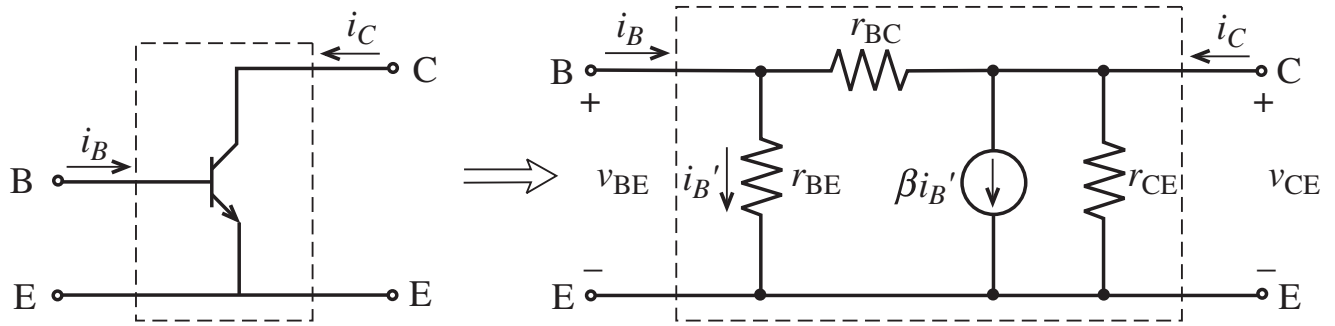


Figure 4-3 Common-emitter low-frequency, small-signal transistor model.

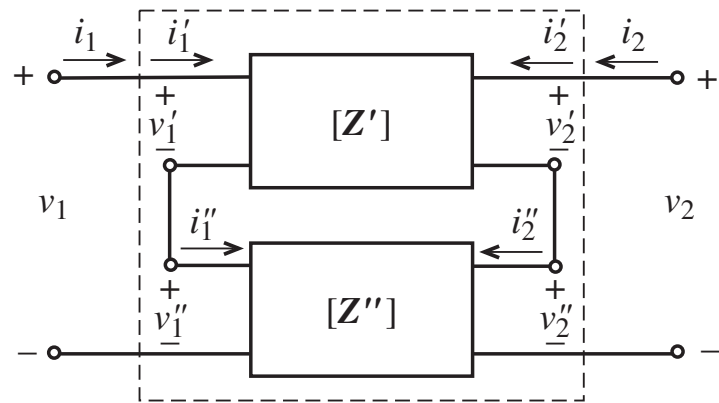


Figure 4-4 Series connection of two two-port networks.

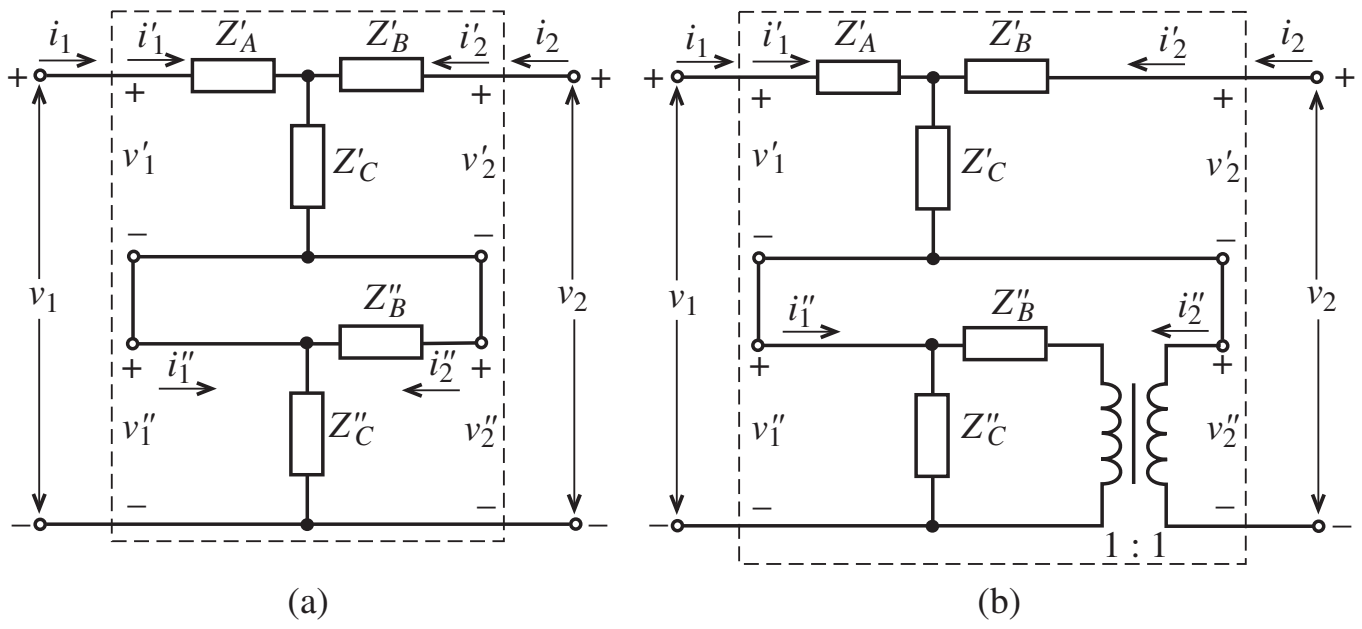


Figure 4-5 (a) Short circuit in series connection. (b) Transformer to avoid short circuit.

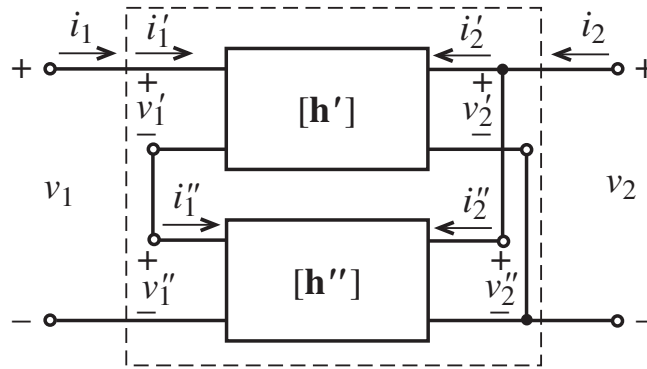


Figure 4-6 Connection of two-port networks suitable for hybrid representation.

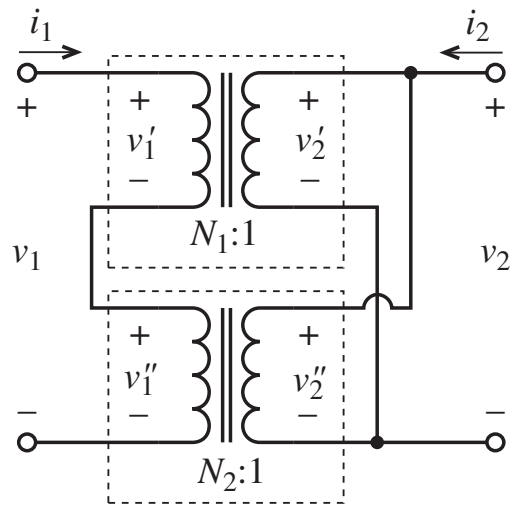


Figure 4-7 Series connection of two hybrid networks.

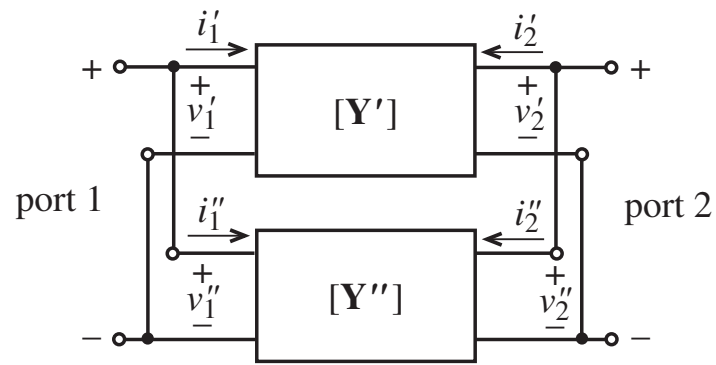


Figure 4-8 Parallel connection of two two-port networks.



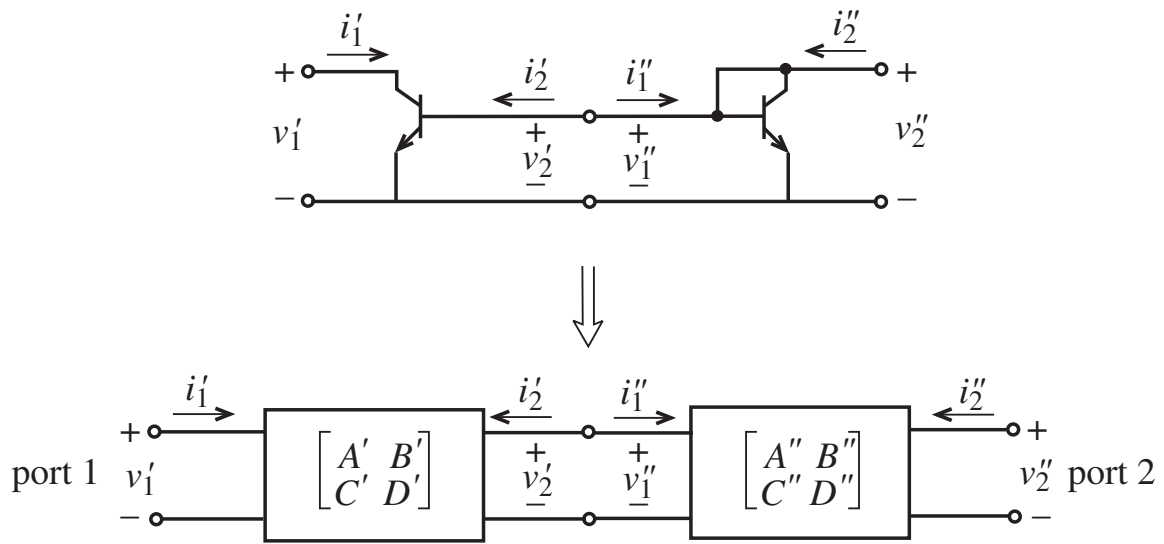


Figure 4-9 Cascading two networks.

Table 4-1 ABCD-parameters of several two-port circuits

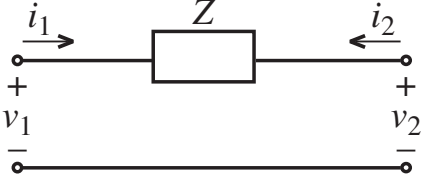
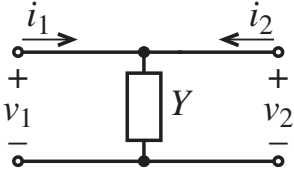
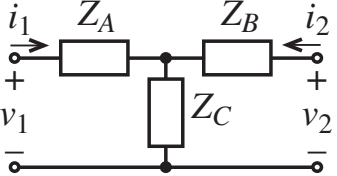
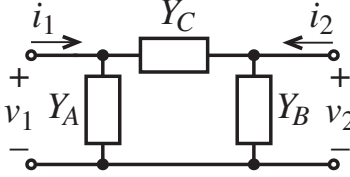
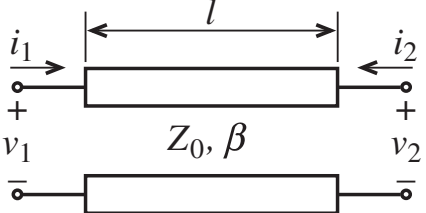
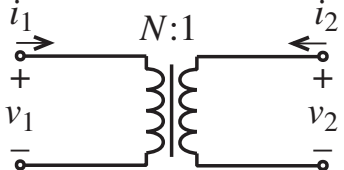
Circuit	ABCD Parameters	
	$A = 1$	$B = Z$
	$C = 0$	$D = 1$
	$A = 1$	$B = 0$
	$C = Y$	$D = 1$
	$A = 1 + \frac{Z_A}{Z_C}$	$B = Z_A + Z_B + \frac{Z_A Z_B}{Z_C}$
	$C = \frac{1}{Z_C}$	$D = 1 + \frac{Z_B}{Z_C}$
	$A = 1 + \frac{Y_B}{Y_C}$	$B = \frac{1}{Y_C}$
	$C = Y_A + Y_B + \frac{Y_A Y_B}{Y_C}$	$D = 1 + \frac{Y_A}{Y_C}$
	$A = \cos(\beta l)$	$B = jZ_0 \sin(\beta l)$
	$C = \frac{j \sin(\beta l)}{Z_0}$	$D = \cos(\beta l)$
	$A = N$	$B = 0$
	$C = 0$	$D = \frac{1}{N}$

Table 4-2 Conversion between different network representations

	[Z]	[Y]	[h]	[ABCD]
[Z]	$\begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix}$	$\begin{bmatrix} \frac{Z_{22}}{\Delta Z} & \frac{Z_{12}}{-\Delta Z} \\ \frac{Z_{21}}{-\Delta Z} & \frac{Z_{11}}{\Delta Z} \end{bmatrix}$	$\begin{bmatrix} \frac{\Delta Z}{Z_{22}} & \frac{Z_{12}}{Z_{22}} \\ \frac{Z_{21}}{Z_{22}} & \frac{1}{Z_{22}} \end{bmatrix}$	$\begin{bmatrix} \frac{Z_{11}}{Z_{21}} & \frac{\Delta Z}{Z_{21}} \\ \frac{1}{Z_{21}} & \frac{Z_{22}}{Z_{21}} \end{bmatrix}$
[Y]	$\begin{bmatrix} \frac{Y_{22}}{\Delta Y} & \frac{Y_{12}}{-\Delta Y} \\ \frac{Y_{21}}{-\Delta Y} & \frac{Y_{11}}{\Delta Y} \end{bmatrix}$	$\begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix}$	$\begin{bmatrix} \frac{1}{Y_{11}} & \frac{Y_{12}}{-Y_{11}} \\ \frac{Y_{21}}{Y_{11}} & \frac{\Delta Y}{Y_{11}} \end{bmatrix}$	$\begin{bmatrix} \frac{Y_{22}}{Y_{21}} & \frac{1}{Y_{21}} \\ \frac{-\Delta Y}{Y_{21}} & \frac{Y_{11}}{Y_{21}} \end{bmatrix}$
[h]	$\begin{array}{cc} \frac{\Delta h}{h_{22}} & \frac{h_{12}}{h_{22}} \\ \frac{h_{21}}{-h_{22}} & \frac{1}{h_{22}} \end{array}$	$\begin{array}{cc} \frac{1}{h_{11}} & \frac{h_{12}}{-h_{11}} \\ \frac{h_{21}}{h_{11}} & \frac{\Delta h}{h_{11}} \end{array}$	$\begin{array}{cc} h_{11} & h_{12} \\ h_{21} & h_{22} \end{array}$	$\begin{array}{cc} \frac{\Delta h}{h_{21}} & \frac{h_{11}}{-h_{21}} \\ \frac{h_{22}}{-h_{21}} & \frac{1}{h_{21}} \end{array}$
[ABCD]	$\begin{array}{cc} \frac{A}{C} & \frac{\Delta ABCD}{C} \\ \frac{1}{C} & \frac{D}{C} \end{array}$	$\begin{array}{cc} \frac{D}{B} & \frac{-\Delta ABCD}{B} \\ \frac{-1}{B} & \frac{A}{B} \end{array}$	$\begin{array}{cc} \frac{B}{D} & \frac{\Delta ABCD}{D} \\ \frac{-1}{D} & \frac{C}{D} \end{array}$	$\begin{array}{cc} A & B \\ C & D \end{array}$

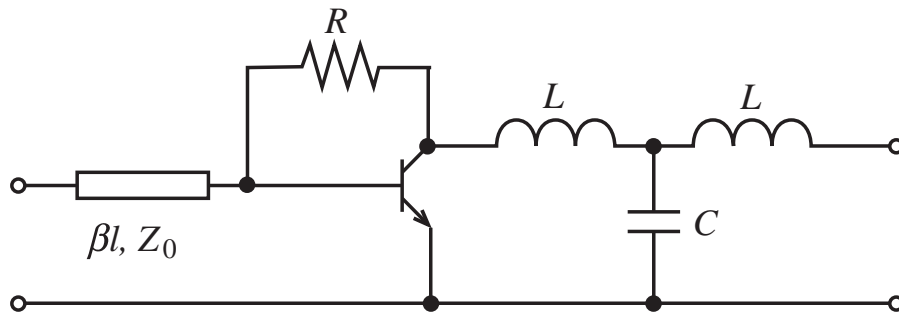


Figure 4-10 Microwave amplifier circuit diagram.

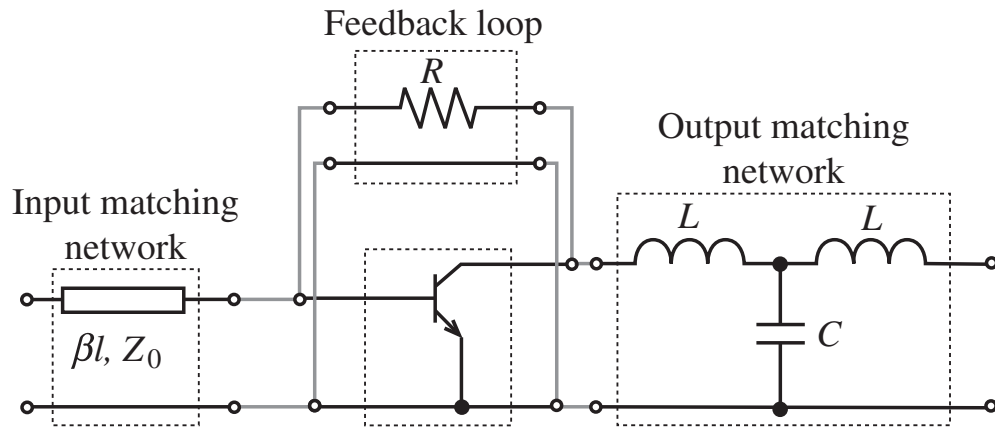


Figure 4-11 Subnetwork representation of the microwave amplifier.

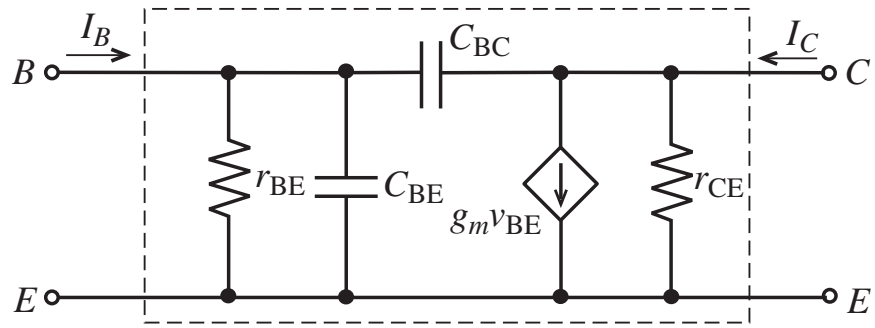


Figure 4-12 High-frequency hybrid transistor model.

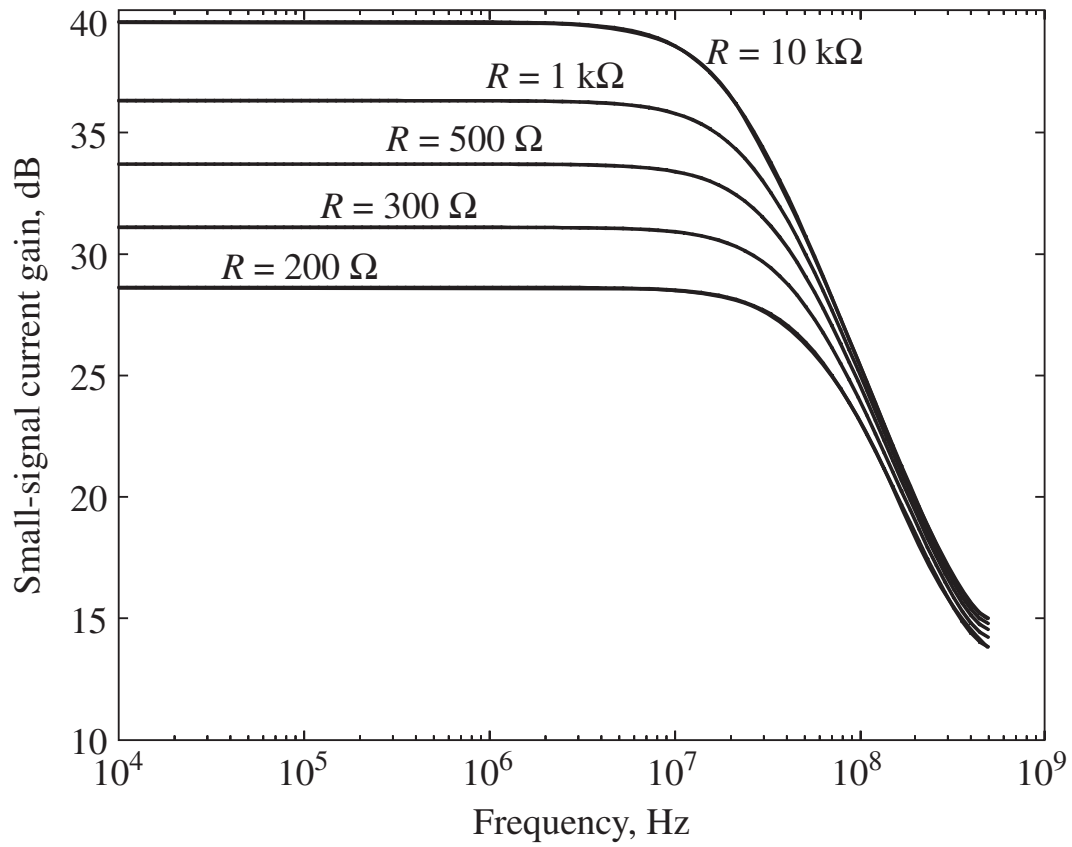


Figure 4-13 Small-signal current gain of the amplifier versus frequency for different values of the feedback resistor.

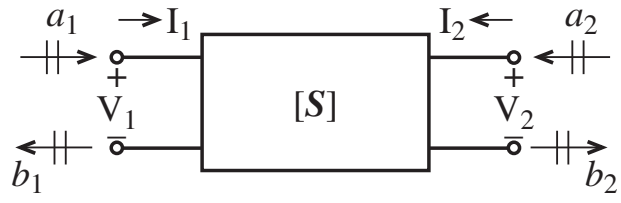


Figure 4-14 Convention used to define S-parameters for a two-port network.



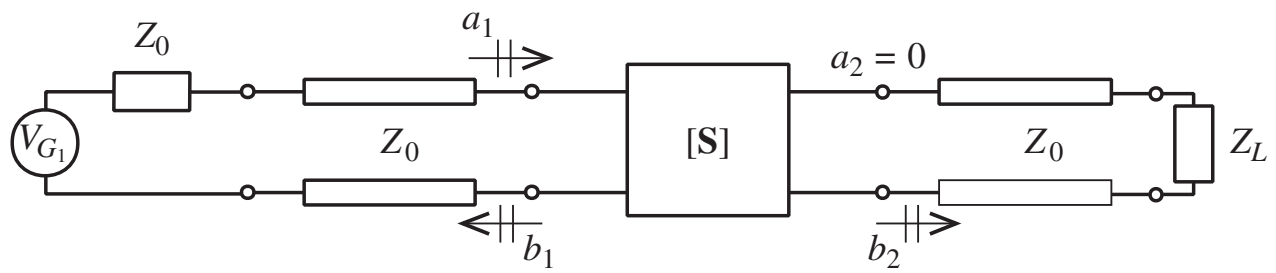


Figure 4-15 Measurement of  $S_{11}$  and  $S_{21}$  by matching the line impedance  $Z_0$  at port 2 through a corresponding load impedance  $Z_L = Z_0$ .

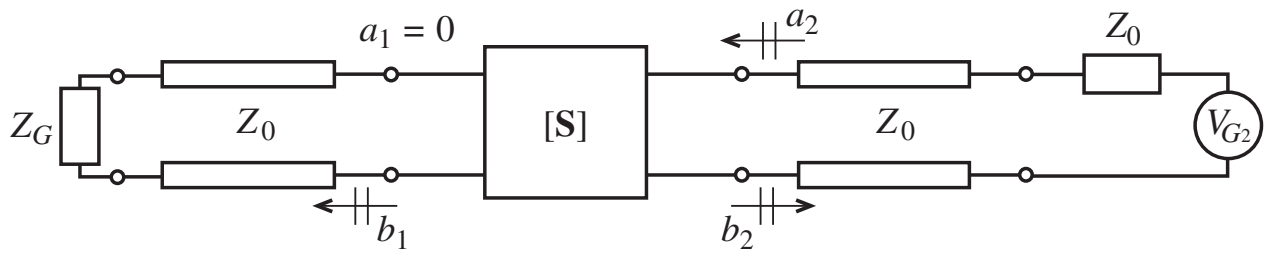


Figure 4-16 Measurement of  $S_{22}$  and  $S_{12}$  by matching the line impedance  $Z_0$  at port 1 through a corresponding input impedance  $Z_G = Z_0$ .

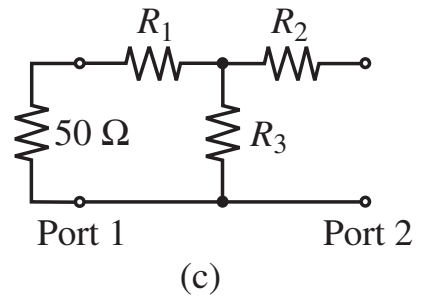
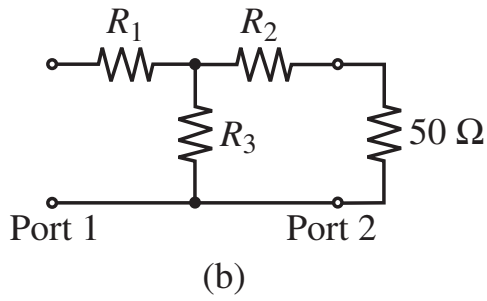
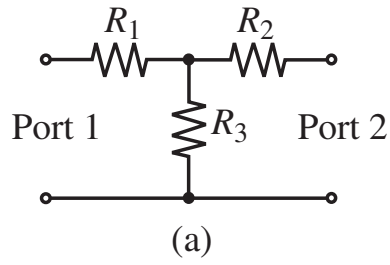


Figure 4-17 S-parameter computation for a T-network.  
 (a) circuit diagram; (b) circuit for  $S_{11}$  and  $S_{21}$  measurements; (c) circuit for  $S_{12}$  and  $S_{22}$  measurements.

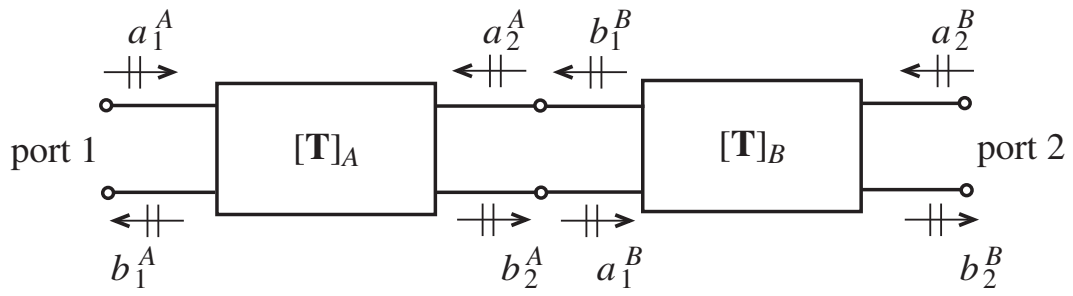


Figure 4-18 Cascading of two networks A and B.

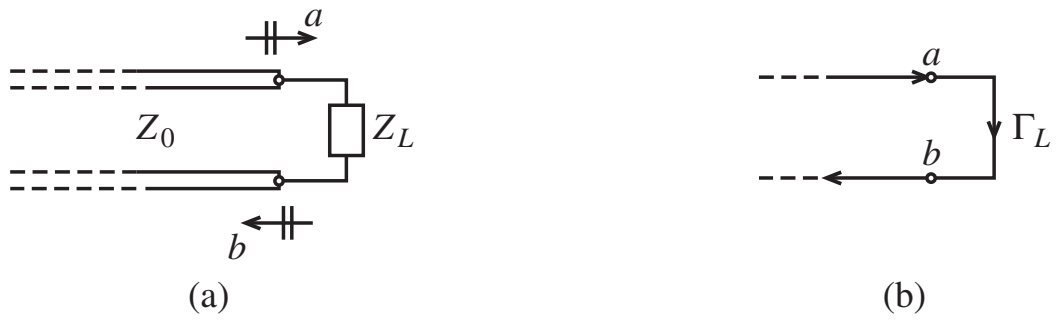


Figure 4-19 Terminated transmission line segment with incident and reflected power wave description. (a) Conventional form, and (b) Signal flow form.



(a) Source node  $a$ , which launches wave.



(b) Sink node  $b$ , which receives wave.



(c) Branch connecting source and sink.

Figure 4-20 Generic source node (a), receiver node (b), and the associated branch connection (c).

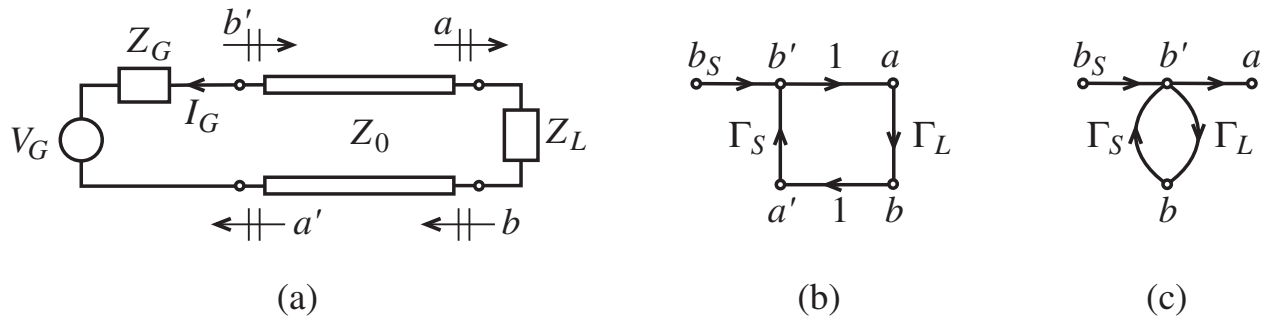


Figure 4-21 Terminated transmission line with source. (a) conventional form, (b) signal flow form, and (c) simplified signal flow form.

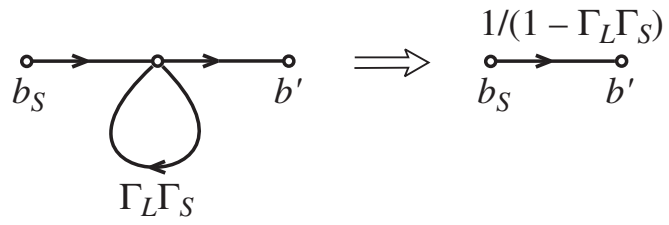
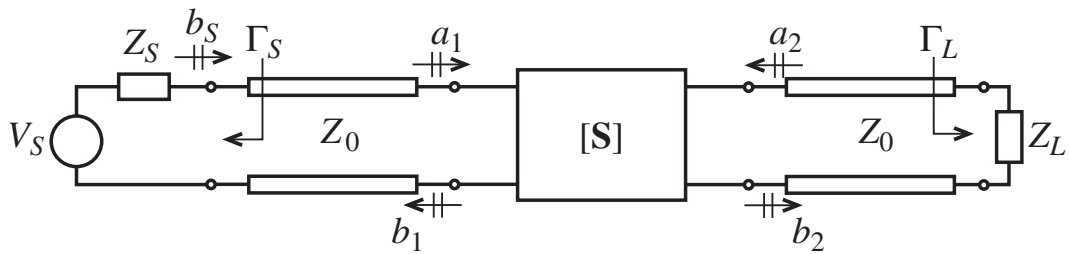


Figure 4-22 A self-loop that collapses to a single branch.

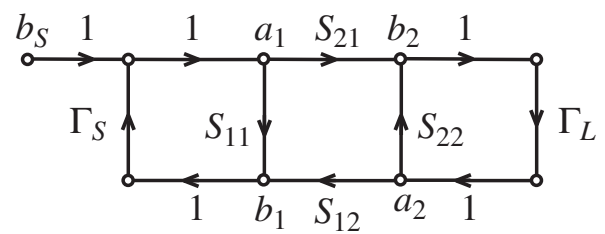


Table 4-3 Signal flowgraph building blocks.

Description	Graphical Representation
Nodal Assignment	
Branch	
Series Connection	
Parallel Connection	
Splitting of Branches	
Self-Loop	

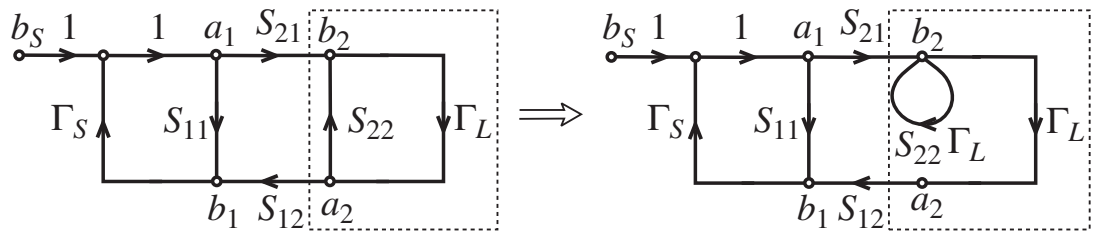


(a) Circuit representation

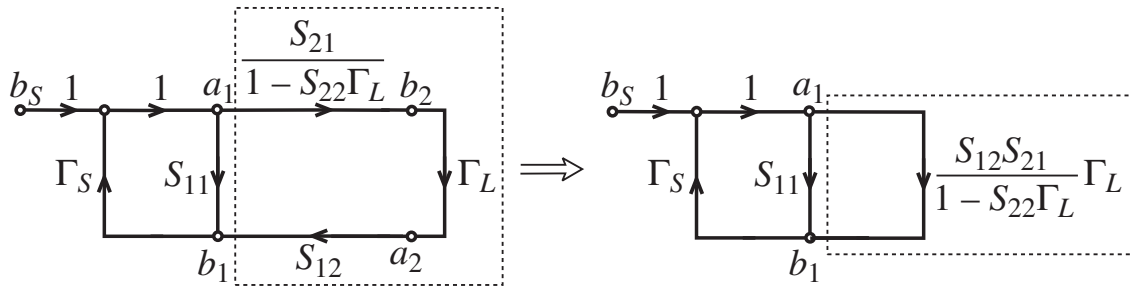


(b) Signal flowgraph

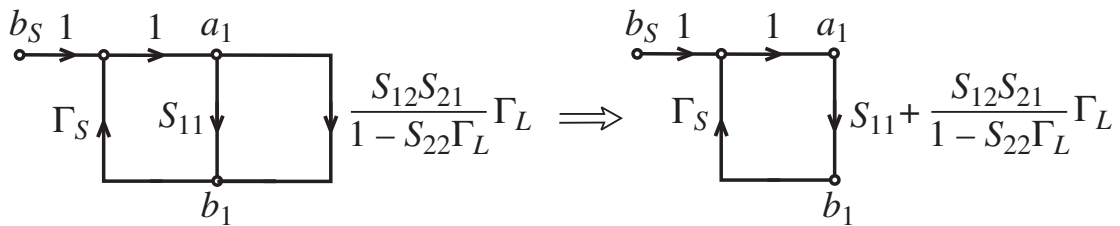
Figure 4-23 Sourced and terminated two-port network.



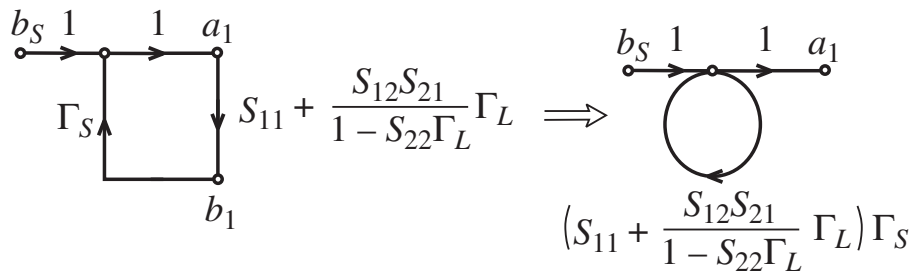
Step 1



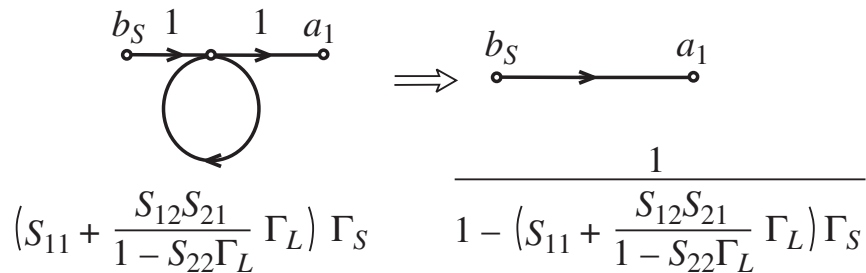
Step 2



Step 3



Step 4



Step 5

Figure 4-24 Step-by-step simplification to determine the ratio  $a_1/b_S$ .

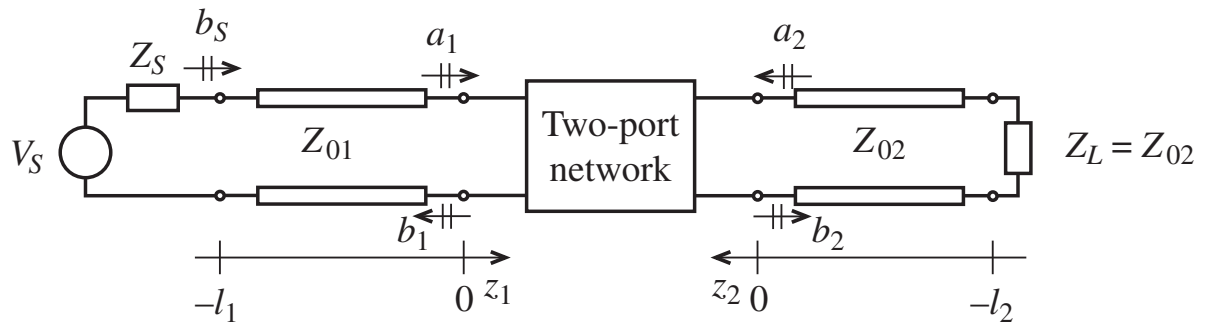


Figure 4-25 Two-port network with finite-length transmission line segments.

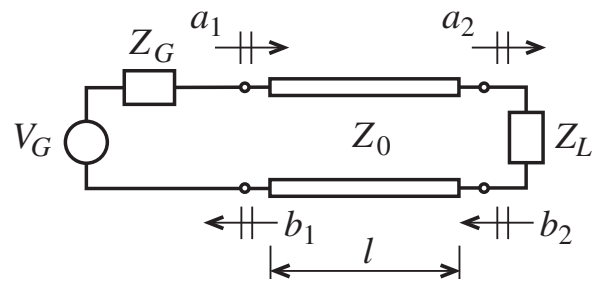


Figure 4-26 Transmission line attached to a voltage source and terminated by a load impedance.

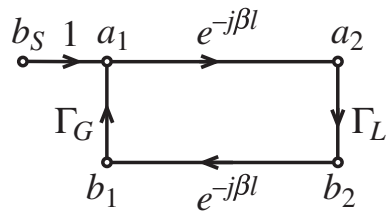


Figure 4-27 Signal flowgraph diagram for transmission line system in Figure 26.

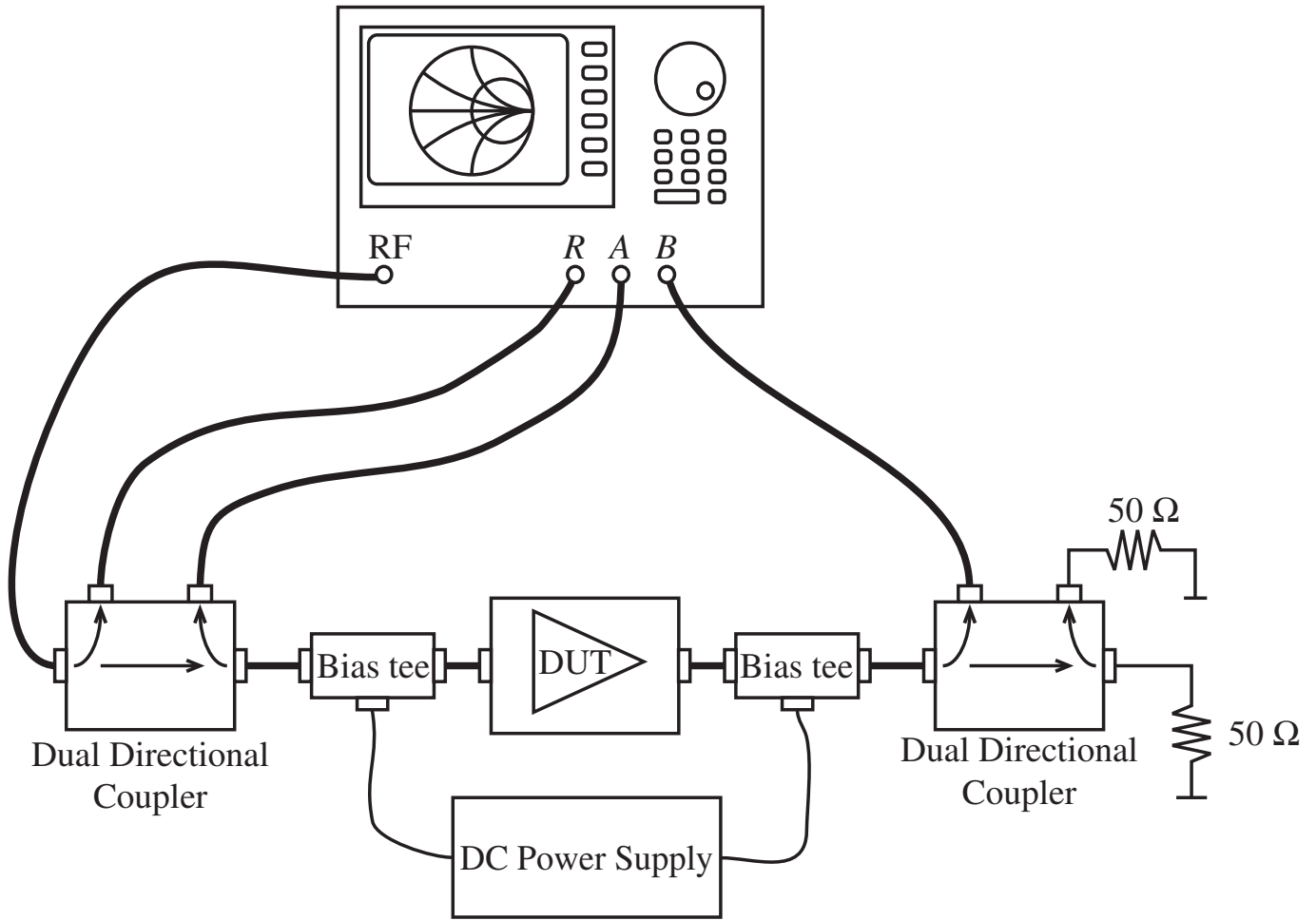


Figure 4-28 Measurement system for  $S_{11}$  and  $S_{21}$  parameters using a network analyzer.

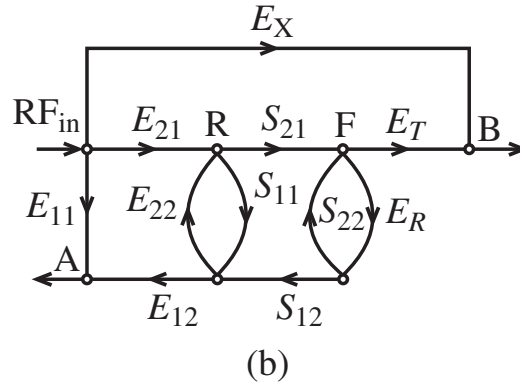
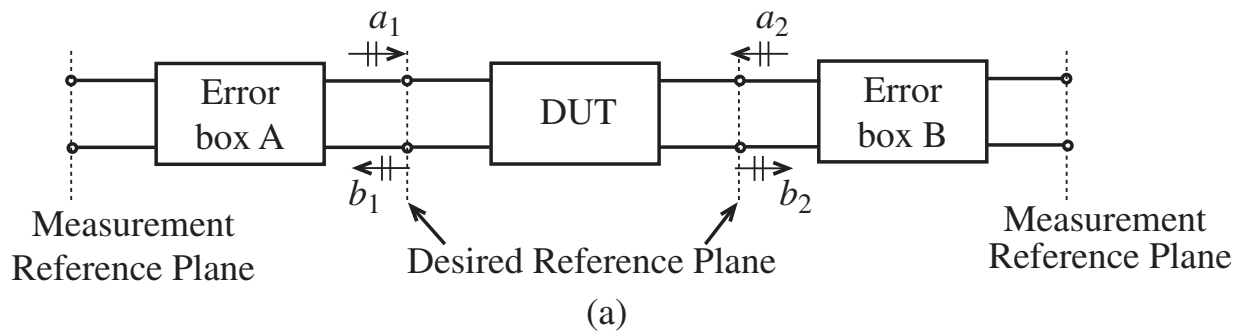
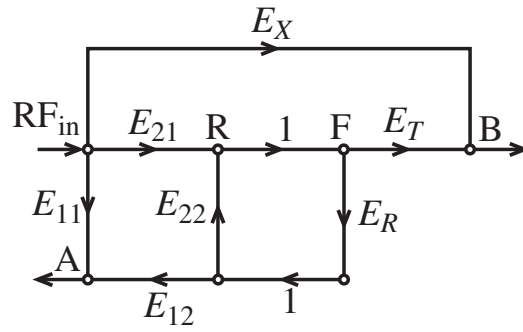
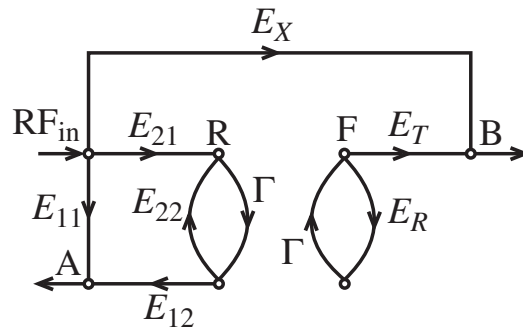


Figure 4-29 (a) Block diagram of the setup for measurement of S-parameters of a two-port network; (b) signal flowgraph of the measurement test setup.

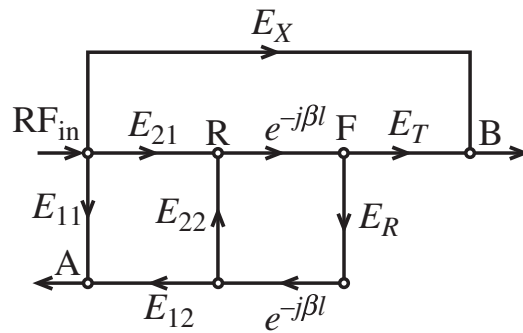




(a) Through



(b) Reflect



(c) Line

Figure 4-30 Signal flow graphs of TRL method: (a) Through, (b) Reflect, (c) Line configurations.

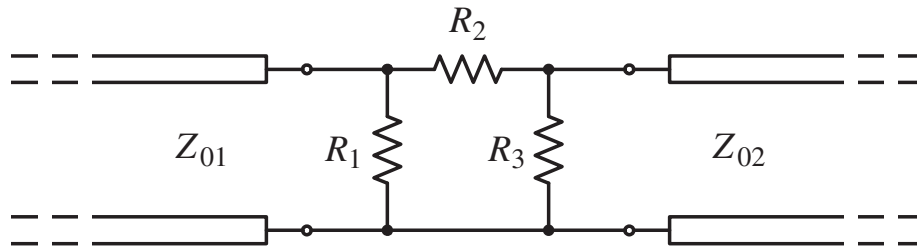


Figure 4-31 Resistive Pi-network attenuator with arbitrary characteristic impedances at the ports.

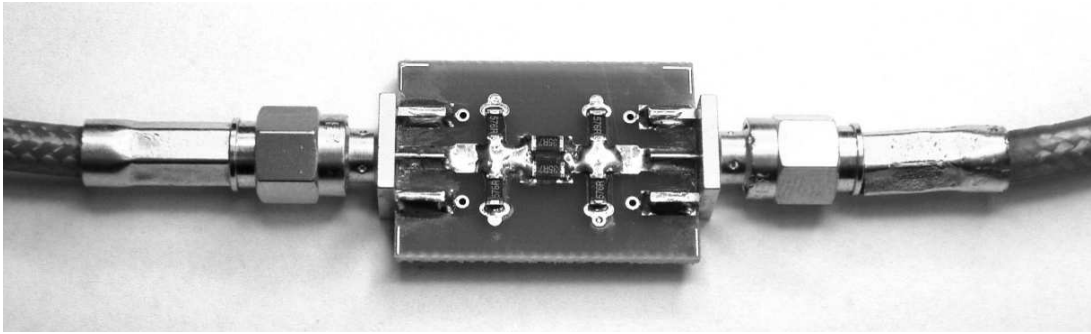


Figure 4-32 Pi-network of a 3 dB attenuator with SMA connectors.

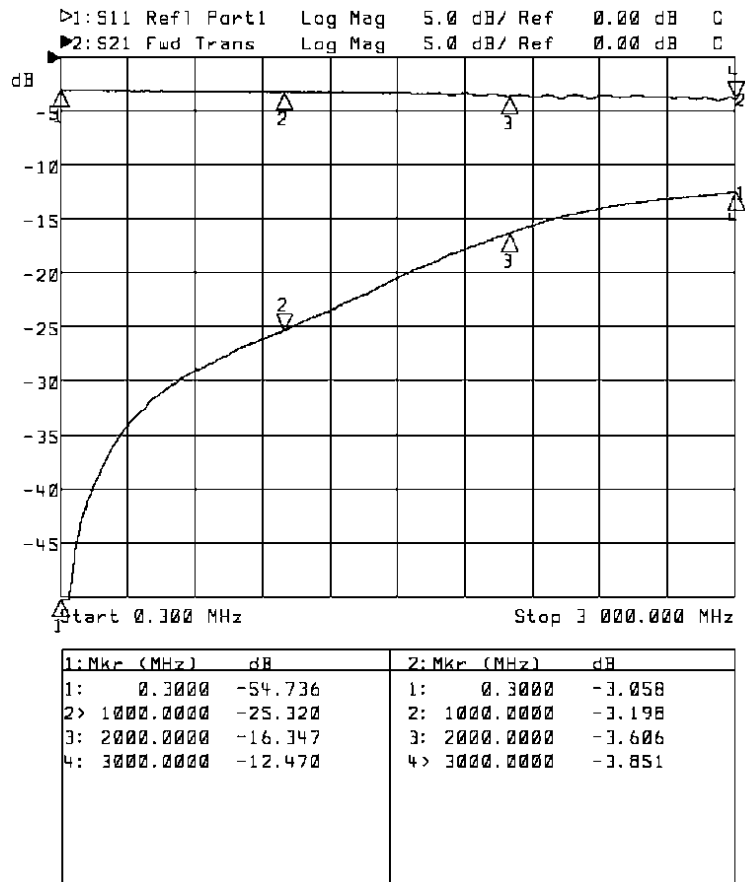


Figure 4-33  $S_{11}$  and  $S_{21}$  recording of the attenuator.